



Figure 1. Physical Photo of ATLS250MA106

### FEATURES

- Ultra Low Noise:  $4.5\mu A_{p-p}$  @ 0.1Hz to 10Hz
- High  $I_{OUT}$  without Heat Sink: 250mA
- High  $I_{OUT}$  Absolute Accuracy: <0.1%
- High  $I_{OUT}$  Stability: <100ppm/°C
- Separate  $I_{OUT}$  and  $I_{OUT}$  limit settings
- Complete Shielding
- Compact Size
- 100 % Lead (Pb)-free and RoHS Compliant
- DIP and SMT Packages Available

### APPLICATIONS

Driving laser diodes with ultra low noise, including DPSSL, EDFA, SOA, fiber laser, DSB diode lasers, etc.

### DESCRIPTION

The ATLS250MA106 is an electronic module designed for driving diode lasers with up to 250mA extra low noise current. Figure 1 shows physical photo of ATLS250MA106. The output voltage is 1.5V to 4V when powered by a 5V power supply.

The controller has temperature compensation network so

that the output current maintains the same even as the controller temperature rises.

In case the controller temperature exceeds a preset limit, 120°C, the controller will be shut down by itself to prevent the controller from being damaged by the over heat.

The output current of the ATLS250MA106 can be set by an input voltage linearly or modulated by an external signal of up to 100kHz in bandwidth, resulting in a minimum 1.5μS rise and fall times at the output current.

A highly stable low noise 2.5V reference voltage is provided internally for setting the output current. This reference can also be used as the voltage reference for external ADCs (Analog to Digital Converters) and/or DACs (Digital to Analog Converters) which are utilized for converting the analog signals, such as LIO which represents the output current, into digital signals, and/or converting the digital signals into analog ones for setting the analog voltages, such as LIS which sets the output current.

The ATLS250MA106 is packaged in a 6 sided metal enclosure, which blocks EMIs (Electro-Magnetic Interferences) to prevent the controller and other electronics from interfering each other.

This laser driver can be evaluated by our evaluation board, [ATLS1A103DEV1.0](#).

There are 2 packaging versions available: DIP through hole package and surface mount type.

**Warning:** Both the surface mount and the through hole types of modules can only be soldered manually on the board by a solder iron of < 310°C (590°F), not go through a reflow oven process.

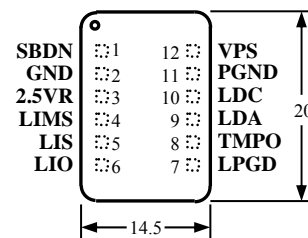


Figure 2. Pin Names and Locations

Figure 2 is the actual size top view of the ATLS250MA106, which shows the pin names and locations. Its thickness is 5mm.

Table 1. Pin Function Descriptions

Pin #	Pin Name	Pin Type	Description
1	SBDN	Digital input	Shut down control. Negative logic. This pin has 3 states: between 0V ~ 0.4V, it shuts down the entire laser driver; between 1.8V ~ 5.5V, it sets the laser driver to operation mode. There is a pull up resistor of 100k connected to the VPS rail.
2	GND	Signal ground	Signal ground pin. Connect ADC and DAC grounds to here.



3	2.5VR	Analog output	2.5V reference voltage. It is used by the internal DACs as the reference voltage. It can source 3mA max, with 5μV <sub>P-P</sub> noise @ 0.1 to 10Hz and 25ppm/°C stability max.
4	LIMS	Analog input	Laser current limit set. 0V to 2.5V sets the laser current limit from 0 to 300mA linearly.
5	LIS	Analog input	Laser current set. 0V to 2.5V sets the laser current from 0 to 250mA linearly.
6	LIO	Analog output	Laser current output indication. 0.1V to 2.5V indicates the laser current of from 0A to 250mA linearly.
7	LPGD	Digital output	Loop good indication. When the controller is working properly, this pin is pulled high by a 4.99k resistor connected to the VPS rail. Otherwise, it is pulled low by an open drain MOSFET, which has the R <sub>dson</sub> of < 100Ω.
8	TMPO	Analog output	The driver internal temperature indication output.
9	LDA	Power output	Laser diode anode. Connect it to the anode of the laser diode. This pin is used to drive the type of diode laser of which the cathode is connected to its case and the case is connected to the ground. See below Figure 4 or Figure 5.
10	LDC	Power output	Laser diode cathode. Connect it directly to the laser's cathode. See below Figure 4 or Figure 5.
11	PGND	Power ground	Power ground pin. Connect it directly to power supply return rail.
12	VPS	Power input	Power supply. The driver works from 3.0V to 5.5V.

### SPECIFICATIONS

Table 2. Characteristics (T<sub>ambient</sub> = 25°C)

Parameter	Value	Unit/Note
Maximum Output Current	250	mA
Output Current Noise (RMS) @ 0.1Hz ~ 10Hz	4.5	μA <sub>P-P</sub>
Current Set Voltage Range (LIS)	0 ~ 2.5	V
Current Limit Set Voltage Range (LIMS)	0 ~ 2.5	V
Bandwidth	200	kHz
Minimum Drop Out Voltage	0.3 + 2.1×I <sub>OUT</sub>	V
Power Supply Voltage Range	3.0 ~ 5.5	V
Operating Case Temperature	-40 ~ 85	°C
Rise and Fall Times	1.5	μS
High I <sub>OUT</sub> Absolute Accuracy:	<0.1%	
High I <sub>OUT</sub> Stability:	<100	ppm/°C

### OPERATION PRINCIPLE

The block diagram of the controller is shown in Figure 3.

The shut down control circuit is activated under one of these 3 circumstances: external shut down, output current exceeds the current limit, and the internal temperature exceeds 120°C.

When the controller is shut down by the external shutdown signal, it will restart upon detecting the releasing of the shutdown signal.

When it is shut down by the over current limit, the controller shuts down itself and restarts again by going through the soft-

start process immediately. Therefore, the output current has a saw-tooth waveform: quick shut down, slow and ramp up.

When the controller is shut down by the over temperature, it will wait till the temperature goes below the temperature limit, 120°C. Usually it takes a few or tens of seconds for the controller to cool down before it restarts itself, depending on the thermal mass of the controller and its surrounding mechanical parts attached thermally, such as the PCB and its traces, the heat-sinks if any, etc.

When controller is shut down, the voltage reference is also shut down.

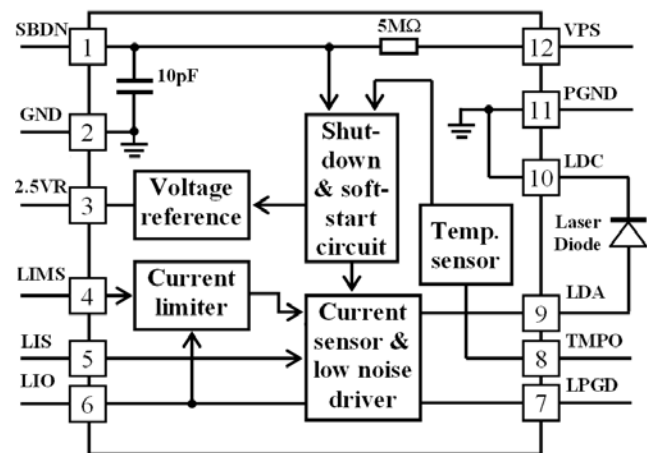


Figure 3. Block Diagram

### APPLICATIONS

Figure 4.1 shows a typical application circuit. W1 and W2 set the output current limit and output current respectively. Resistor R1 and capacitor C1 form a low pass filter, to lower the noise from the voltage reference.

Laser diode D1 is connected between LDA and PGND. It is worth mentioning that the power supply return terminal should be connected to the pin 11 PGND and the cathode of the laser diode should be connected to the pin 10 LDC. These 2 nodes should not be connected together externally and they are connected together internally already by the controller.

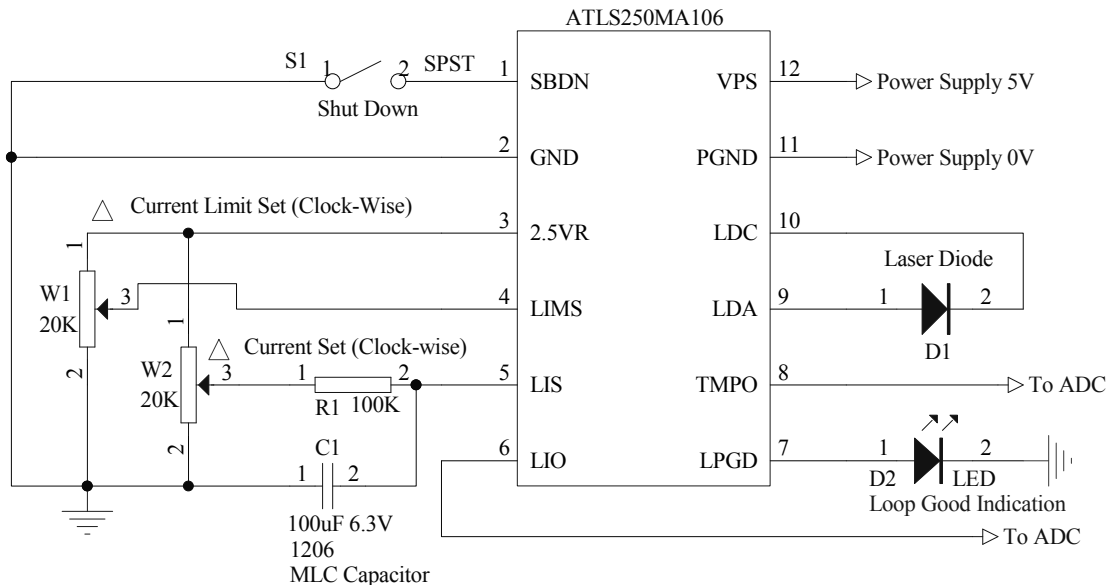


Figure 4.1. Typical Stand-alone CW Operation Schematic for ATLS250MA106

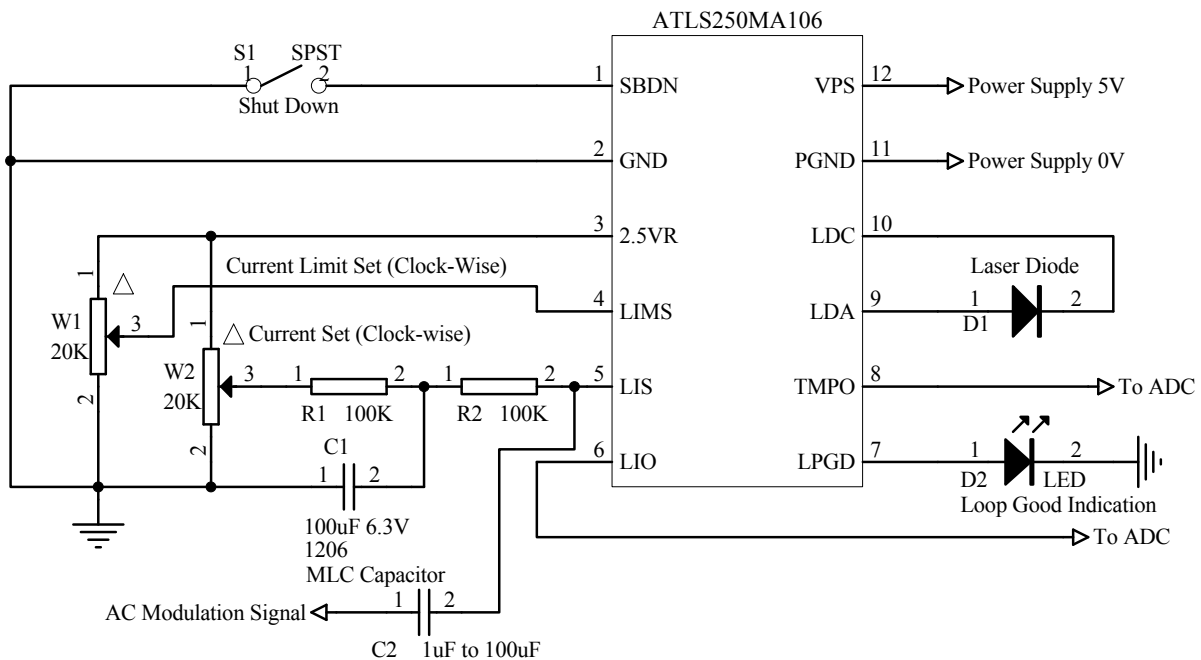


Figure 4.2. Typical AC Modulation with DC bias Schematic for ATLS250MA106



#### Turning the Controller On and Off

The controller can be turned on and off by setting the SBDN pin high and lower respectively. It is recommended to turn the controller on by this sequence:

**To turn on:** turn on the power by providing the power supply voltage to the controller, turn on the controller by releasing the SBDN pin.

**To turn off:** turn off the controller by lowering the voltage of SBDN pin, turn off the power by stopping the voltage supply on the VPS pin.

When not controlling by the SBDN pin: leave it unconnected and turn on and off the controller by the power supply.

In Figure 4.1, S1 is the shut down switch. The internal equivalent input circuit of SBDN pin is a pull-up resistor of 100k being connected to VPS in parallel with a 10pF capacitor to the ground. The switch S1 can also be an electronic switch, such as an I/O pin of a micro-controller, with an either open drain or push/pull output. If not using a switch (S1) to control the laser, leave the SBDN pin unconnected. D2 is an LED, indicating when the control loop works properly, that is: the output current equals to the input set value. This pin has an internal pull up resistor of 5k to the power supply pin, VPS, pin 10. The pull down resistance is 200Ω. This 5k resistor can drive a high efficiency LED directly. When higher pull up current is needed for driving such as a higher current LED, an external resistor can be placed between the VPS and the LPGD pins. Make sure that the resistor is not too small that the pull down resistor will not be able to pull the pin low enough when the controller loop is not good. When choosing not to use an LED for indicating the working status, leave the LPGD pin unconnected.

The LPGD pin can also be connected to a digital input pin of a micro-controller, when software/firmware is utilized in the system.

#### Setting the Output Current

The output current limit is set by adjusting W1, which sets input voltages of LIMS, pin 4. The output current will be:

$$I_{OUT} \approx 300 \times LIMS (V)/2.5V (mA).$$

$$I_{OUT} = (LIMS (V) - 0.1)/(8 \times 10^{-3}) (mA).$$

LIMS should never be left float. Otherwise, the output current limit may be set to too high a value that the laser might be damaged.

The output current is set by adjusting W2, which sets input voltages of LIS, pin 5. The output current will be:

$$I_{OUT} \approx 250 \times LIS (V)/2.5V (mA).$$

$$I_{OUT} = (LIS (V) - 0.1)/(9.6 \times 10^{-3}) (mA).$$

When no modulation is needed, it is suggested to use an RC low-pass-filter, the R1 and C1 in Figure 4.1, to lower the AC noise from the voltage reference source. The time constant of this filter can be between a few to 10's of seconds. The bigger the time cost, the lower the output noise, but the longer time will be needed to wait the output current to go up.

Both of LIMS and LIS, only LIS, can be configured by using a DAC, to replace the W1 and W2 in Figure 4.1. Make sure that the DAC has output low noise, or, if no modulation is needed, an RC low pass filtered by be inserted between the DAC and the LIS pin, similar as shown in Figure 4.1.

The LIS allows modulating the output current by a signal of up to 100kHz in bandwidth. That is, when using a sine wave signal to modulate the LIS pin, the output current response curve will be attenuated by 3dB, or 0.707 times the full response magnitude in current. When using an ideal square-wave to modulate the output current at the LIS pin, the rise and fall time of the output current will be about 1.5μS.

When the modulation signal is a square-wave and low output noise is require, the low-pass-filter can still be used for lowering the output noise. Figure 5 shows such a circuit. The resistor R1 can be 10k to 1M, depending on the error voltage caused by the switch leakage current. The LIMS pin can be set by a POT as shown in Figure 5 or connect to 2.5VR.

It is recommended not to set the LIS pin to 0V, but keep it >0.05V at all the time. The reason is that the laser diode usually has a junction voltage of 2.5V, when setting the LIS pin voltage to 0V, the output voltage will warble between 0V and 2.5V, cause some oscillation slightly.

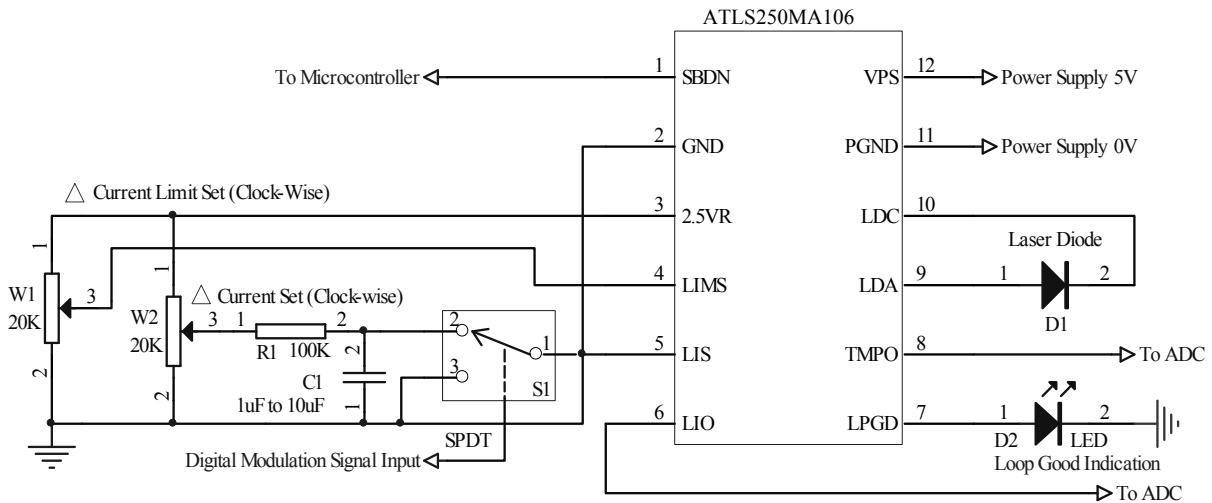


Figure 5. Low Noise Digital Modulation Circuit

The LIO can still be used to monitor the output current when the LIS is modulated. The bandwidth of the LIO signal is up to 9.17MHz, more than enough for monitoring output current modulated by the LIS signal.

### Monitoring the Output Current

The output current of the controller can be monitored by measuring the voltage on the LIO pin. This feature is very useful for micro-controller based system where the ADC is available and monitoring the current in real time is required. This pin provides a very low noise voltage signal which is proportional to the output current:

$$LIO (V) = I_{OUT} \times 10 (V).$$

For example, when the output signal equals to 2.5V, the output current is 250mA.

The output impedance of this pin is 10Ω and it can be used to drive an ADC directly.

It can also be measured by a multimeter during debugging process.

Figure 6 below shows the relations among LIS, LIMS and  $I_{OUT}$

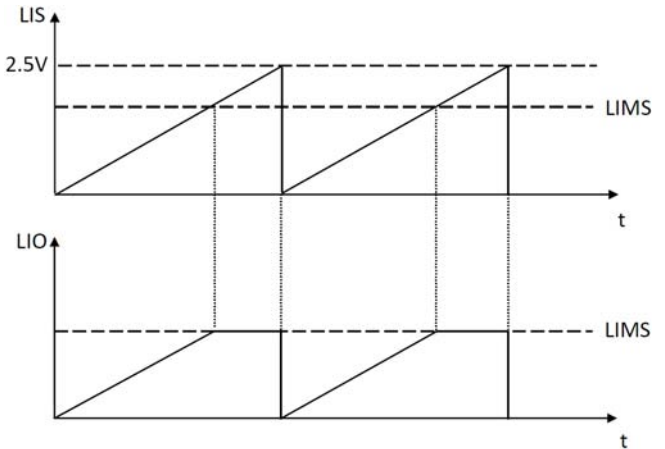


Figure 6. LIO is Controlled by LIS and Clamped by LIMS

When the output current set by LIS is less than the current limit set by LIMS, the actual output current  $I_{OUT}$  changes with LIS linearly; when output current set by LIS exceeds the current limit set by LIMS,  $I_{OUT}$  will be clamped to the value set by the LIMS, see Figure 6.

### Monitoring the Controller Internal Temperature

The controller internal temperature can be monitored by measuring the TMPO pin voltage. The relationship between the LMPO voltage and the temperature is:

$$T = -1525.04 + 10^3 \sqrt{2.4182 + \frac{1.8015 - TMPO}{3.479}} (^\circ C) \quad (1)$$

where TMPO is the voltage on the TMPO pin.

This formula can be approximated by a linear equation:

$$T = 192.7 - 90.31 \times TMPO (^\circ C) \quad (2)$$

Within the most commonly used temperature range of between 0°C to 100°C, the maximum error occurs at about 1.5V, at which the temperature error between the





calculated data by using the formula (1) and the approximated data obtained by using the linear equation (2) is about 0.4°C, with the linear data being a little lower. The curves of the 2 sets of the data are plotted in Figure 15.

Please notice that the TMPO pin has a weak driving capability: the maximum sourcing current is 1μA and the maximum sinking current is 40μA.

The TMPO pin can also be used as an input control pin: when forcing the TMPO voltage to below 0.4V, the laser controller will be shutdown.

### Controller Power Consumption

When the maximum power consumed by the controller is maintained to <1W, it does not require a heat sink to operate. The power dissipated by the controller can be calculated by this formula:

$$I_{VPS} = I_Q + I_{OUT}$$

$$P_{IN} = V_{VPS} \times I_{VPS}$$

$$P_{OUT} = V_{OUT} \times I_{OUT}$$

$$P_{DRIVER} = P_{IN} - P_{OUT}$$

$$= V_{VPS} \times I_Q + V_{VPS} - V_{OUT}) \times I_{OUT}$$

Where  $I_{VPS}$  is the input current at the VPS node,  $V_{VPS}$  is the power supply voltage,  $I_{GND}$  is the ground pin current,  $V_{OUT}$  is the output voltage at the load,  $I_{OUT}$  is the output current going through the load.

Figure 7 shows the current distributions of the controller.

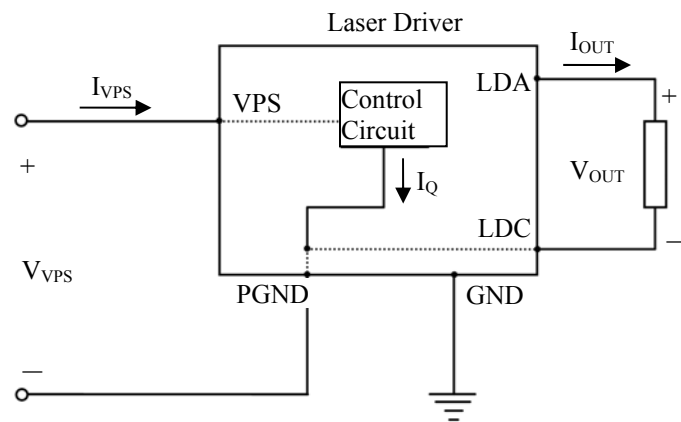


Figure 7. The Current Distributions in the Controller

When the  $P_{DRIVER}$  exceeds 1W, a heat sink might be needed. Under this situation, if prefer not to use the heat sink, this is an option: lowering the controller power consumption by reducing the power supply voltage  $V_{VPS}$ . Please make sure:

$$V_{VPS} \geq V_{OUTMAX} + 1V,$$

where  $V_{OUTMAX}$  is the maximum possible laser diode voltage.

### First Time Power Up

Laser is a high value and vulnerable device. Faults in connections and damages done to the controller during soldering process may damage the laser permanently.

To protect the laser, it is highly recommend to use 3 to 4 regular diodes of >200mA to form a “dummy laser” and insert it in the place of the real laser diode, when powering up the controller for the first time. Use an oscilloscope to monitor the LDA voltage at times of power-up and power-down, make sure that there is not over-shoot in voltage. At the same time, use an ammeter in serious with the dummy laser, to make sure that the output current is correct.

After thorough checking free of faults, disconnect the dummy laser and connect the real laser in place.

The controller output voltage range for the laser is between 0.5 to 4V when powered by a 5V power supply.

### Bandwidth Measurement

The controller bandwidth is 100kHz. There are two methods to measure the bandwidth: large signal modulation and small signal modulation. The measuring methods are as below.

#### Small Signal Modulation Definition

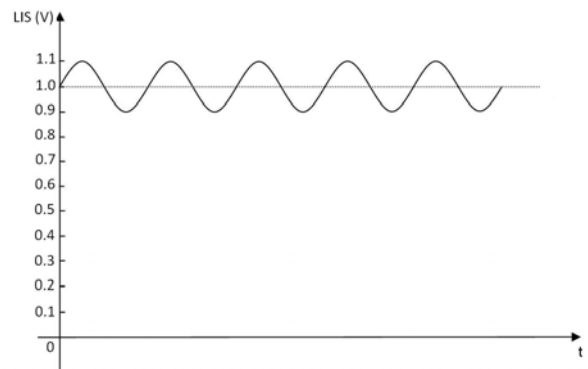


Figure 8.1 Small Signal Modulation

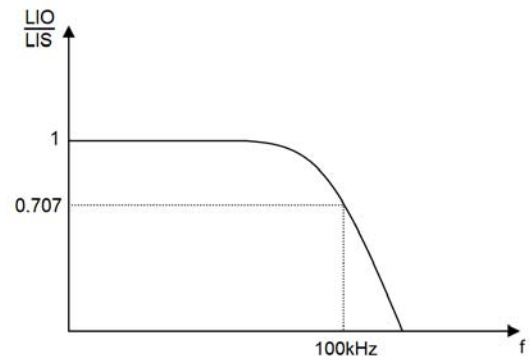


Figure 8.2. The Ratio of LIO/LIS

As shown in Figure 8.1, add a sine signal of 1V DC + 0.2 V<sub>P-P</sub> AC (the frequency increases generally) to LIS and then measure the AC voltage on LIS and LIO. The AC voltage ratio of LIO (AC)/LIS (AC) is 0.707 at the frequency of around 200kHz, see Figure 8.2

### Large Signal Modulation Definition

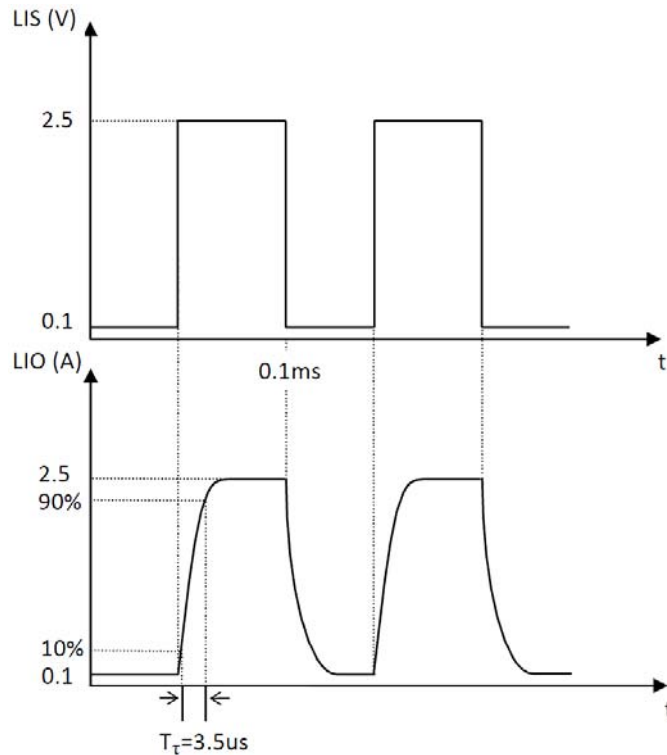


Figure 9. Large Signal Modulation

As shown in Figure 9, when a square wave of 0.1V~2.5V,  $f = 100\text{Hz}$ , is applied to LIS, measure the waveform of LIO. The rise and fall time should be about  $1.5\mu\text{s}$ , the equivalent bandwidth can be calculated by:

$$f = 0.35/t_{\text{rise}} = 0.35/1.5\mu\text{s} = 200\text{kHz}.$$

The above two methods can be applied to test if the bandwidth is 200kHz.

In practice, the small signal bandwidth is usually much higher than the large signal bandwidth.

### MECHANICAL DIMENSIONS AND MOUNTING

The ATLS250MA106 comes in 2 packages: through hole mount and surface mount. The former is often called DIP (Dual Inline package) or D (short for DIP) package and has a part number: ATLS250MA106-D, and the latter is often called SMT (Surface Mount Technology) or SMD (Surface Mount Device) package and has a part number: ATLS250MA106-S. See below Figure 10 and 11.

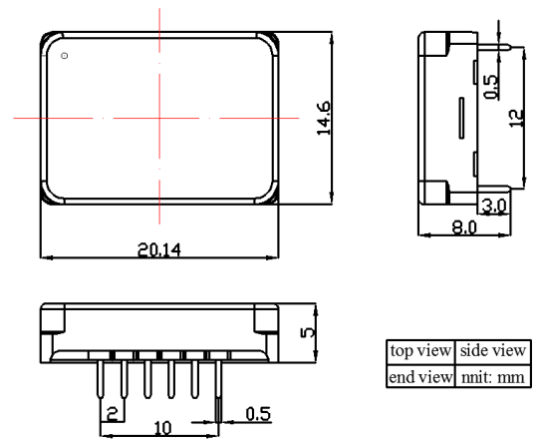


Figure 10. Dimensions of the DIP Package Controller

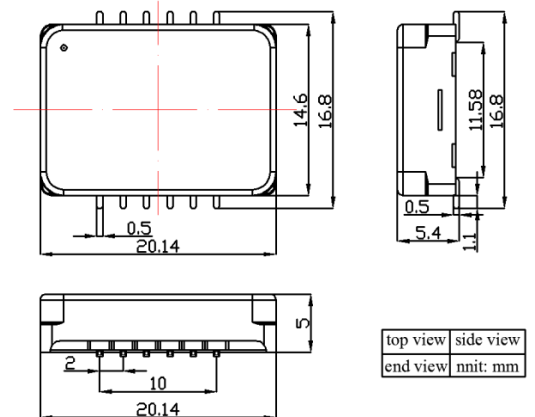


Figure 11. Dimensions of the SMT Package Controller

“Tent” (i.e. cover the entire via by the solder mask layer) all the vias under the controller, otherwise, the vias can be shorted by the bottom plate of the controller which is internally connected the ground.

Please notice that, in the recommended foot print for the DIP package, the holes for pin 2 to 6, and 8 to 12 have larger holes than needed for the pins. This arrangement will make it easier for removing the controller from the PCB, in case there is a rework needed. The two smaller holes, for pin 1 and 7, will hold the controller in the right position.

It is also recommended to use large copper fills for VPS, PGND, and the LDC pins, and other pins if possible, to



decrease the thermal resistance between the module and the supporting PCB, to lower the module temperature.

Please be notice that the SMT version cannot be soldered by reflow oven. It must be soldered manually.

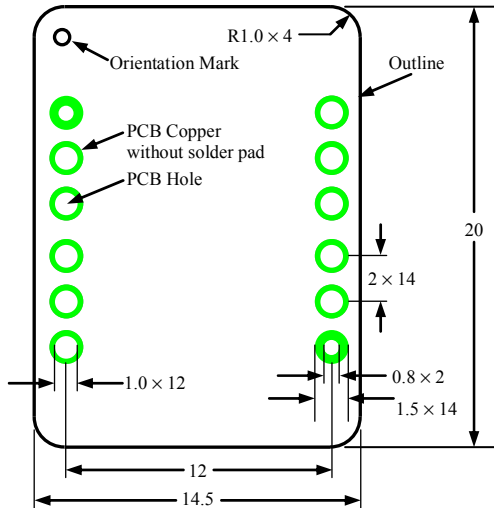


Figure 12. Top Side PCB Foot-print for the DIP Package

Figure 12 shows the foot print which is seen from the top side of the PCB, therefore, it is a “see through” view.

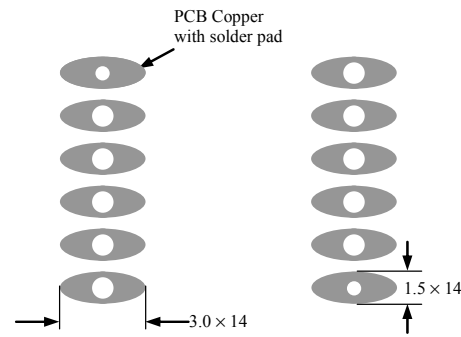


Figure 13. Top View of the Bottom Side PCB Foot-print

Figure 13 shows the view of the bottom side PCB foot-print.

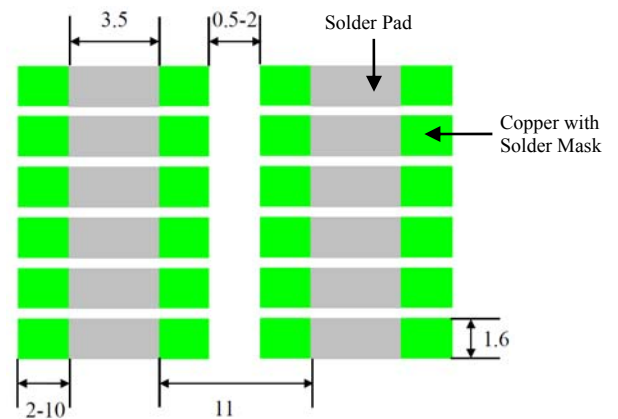


Figure 14. Top View of the Bottom Side of Surface Mount PCB Foot-print

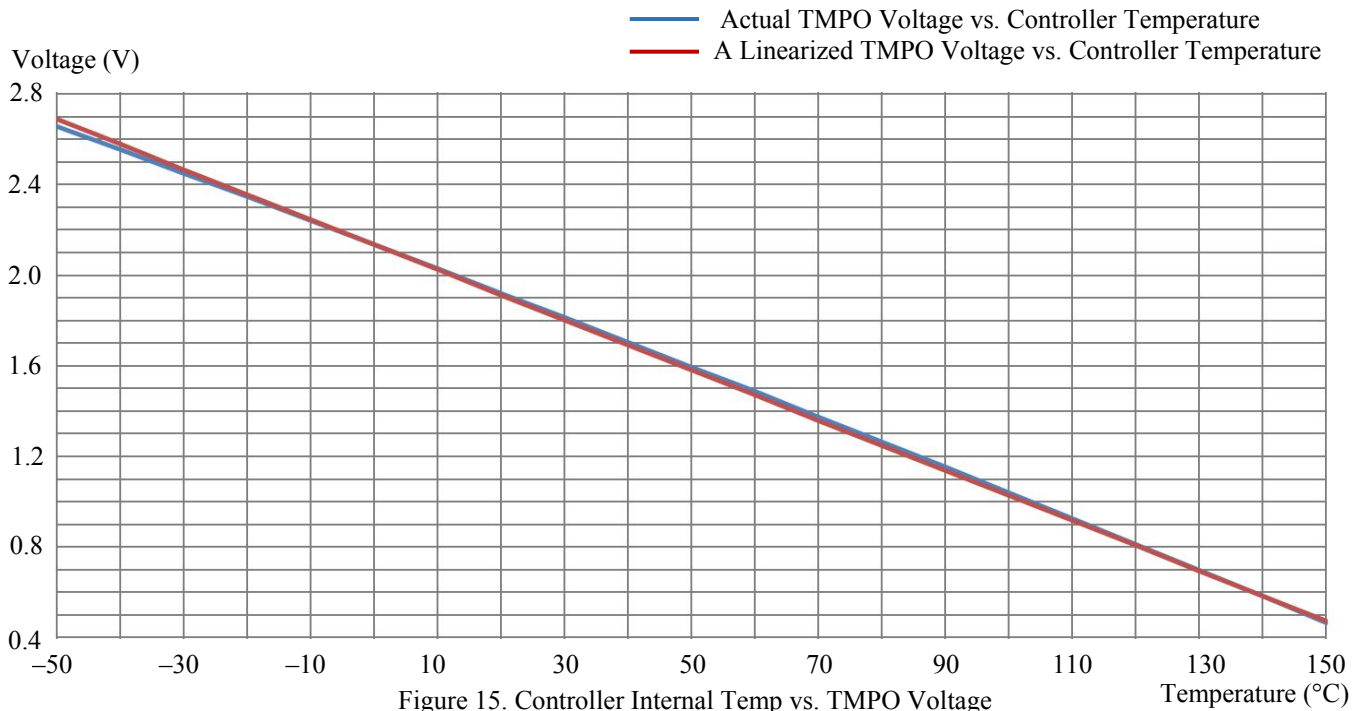


Figure 15. Controller Internal Temp vs. TMPO Voltage





# Low Noise Constant Current Laser Controller

## ATLS250MA106

**WARNING:** Both the surface mount and the through hole types of modules can only be soldered manually on the board by a solder iron of < 310°C (590°F), not go through a reflow oven process.

**NOTE:** The power supply may have overshoot, when happens, it may exceed the maximum allowed input voltage, 6V, of the controller and damage the controller permanently. To avoid this from happening, do the following:

1. Connect the controller solid well with the power supply before turning on the power.
2. Make sure that the power supply has sufficient output current. It is suggested that the power supply can supply 1.2 to 1.5 times the maximum current the controller requires.
3. When using a bench top power supply, set the current limit to >1.5 times higher than the maximum current the controller requires.
4. This laser driver can be evaluated by our evaluation board, [ATLS1A103DEV1.0](#).

### ORDERING INFORMATION

Table 3. Part Number

Part #	Description
ATLS250MA106-D	Controller in DIP package
ATLS250MA106-S	Controller in SMT package

Table 4. Unit Price

Quantity	1 – 9	10 – 49	50 – 199	200 – 499	≥500
ATLS250MA106-D ATLS250MA106-S	\$75	\$69.5	\$65	\$61	\$58

### SELECTION GUIDE

Part #	Ultra Low Noise	Rise and Fall Times	Standby	Shut down
ATLS250mA104	1.98μV <sub>P-P</sub>	100nS	Yes	Yes
ATLS250mA106	4.5μV <sub>P-P</sub>	1.5μS	No	Yes
ATLS250mA103	2.5μV <sub>P-P</sub>	300nS	No	Yes

\*Total RMS between 0.1Hz to 10Hz.



**NOTICE**

1. ATI warrants performance of its products for one year to the specifications applicable at the time of sale, except for those being damaged by excessive abuse. Products found not meeting the specifications within one year from the date of sale can be exchanged free of charge.
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